Corrigenda

Anisotropy of small strain stiffness in Ticino sand by R. Bellotti, M. Jamiolkowski, D. C. F. Lo Presti and D. A. O'Neill (1996). *Geotechnique* **46**, No. 1, 115–131

On page 119, Equation (3) *should read*:

$$V_s = C_s[F(e)]^{0.5}(\sigma'_a)^{na} \cdot (\sigma'_b)^{nb} \cdot (\sigma'_c)^{nc}$$

and Equation (4) *should read*:

$$V_p = C_p[F(e)]^{0.5}(\sigma'_a)^{na} \cdot (\sigma'_b)^{nb} \cdot (\sigma'_c)^{nc}$$

On page 125, left-hand column, line 36, Table 4 *should read* Table 5.

On page 126, right-hand column, line 2, (not measured during this research) *should read* (only the latter has been measured during this research).

On page 130, left-hand column, line 1, by the poor sensitivity of the method *should read* by the sensitivity of the method to possible experimental errors.

On page 130, left-hand column, line 3, $na = nb = 0.25$ *should read* $na = nb = 0.125$.

On page 130, left-hand column, line 15, The sensitivity of this approach *should read* The reliability of this approach.

On page 130, right-hand column, line 20, the poor sensitivity of the method *should read* the extreme sensitivity of the method to even small experimental errors.

On page 121, left-hand column, caption text for Fig. 7 and 8 was inverted and *should read* as follows:

Fig. 7. Velocity of compression waves polarized in the horizontal plane

Fig. 8. Velocity of shear waves polarized in the horizontal plane

A compression model for non-brittle soft clays and peat by E. J. Den Haan (1996). *Geotechnique* **46**, No. 1, 1–16

On page 5, right-hand column, line 3, Equation (15)

$$q = -\frac{\gamma_s - \gamma_w v_0}{\gamma_w} \frac{\partial}{\partial z} \left(\frac{k}{v} \right) + \frac{1}{\gamma} \frac{v_0}{v} \frac{\partial}{\partial z} \left[\frac{k v_0}{v} \frac{\partial \sigma'_v}{\partial z} \right]$$

should read

$$q = -\frac{\gamma_s - \gamma_w v_0}{\gamma_w} \frac{\partial}{\partial z} \left(\frac{k}{v} \right) + \frac{1}{\gamma_w} \frac{v_0}{v} \frac{\partial}{\partial z} \left[\frac{k v_0}{v} \frac{\partial \sigma'_v}{\partial z} \right]$$

Equation (18)

$$\frac{d\sigma'_v}{dt} = \frac{\partial'_v}{a} \left[-\frac{\gamma_s - \gamma_w v_0}{\gamma_w} \frac{\partial}{\partial z} \left(\frac{k}{v} \right) + \frac{1}{\gamma_w} \frac{v_0}{v} \frac{\partial}{\partial z} \left(k \frac{v_0}{v} \frac{\partial \sigma'_v}{\partial z} \right) - \frac{c}{\tau} \right]$$

should read

$$\frac{d\sigma'_v}{dt} = \frac{\partial'_v}{a} \left[-\frac{\gamma_s - \gamma_w v_0}{\gamma_w} \frac{\partial}{\partial z} \left(\frac{k}{v} \right) + \frac{1}{\gamma_w} \frac{v_0}{v} \frac{\partial}{\partial z} \left(k \frac{v_0}{v} \frac{\partial \sigma'_v}{\partial z} \right) - \frac{c}{\tau} \right]$$

On page 7, right-hand column, Fig. 5 caption text, Zegfeld *should read* Zegveld.

On page 8, right-hand column, Fig. 7 caption text, **Constrained modulus M plotted against σ'_v on $\tau = 1$ day isotaches Figs 4(a) and 5(a) *should read* Constrained modulus M versus σ'_v on $\tau = 1$ day isotaches in (Figs 4(a) and 5(a)).**

On page 10, left-hand column, line 18 Fig. 8(a) *should read* Fig. 8(b).

On page 11, right-hand column, line 10–11; Some models do not include direct compression, equation (23) then reduces to *should read* Some models do not include direct compression. Equation (23) then reduces to; Line 40, *Rate against time **should read** Rate versus time.*

On page 12, left-hand column, line 53, mode *should read* model.

On page 8, left-hand column, Fig. 6 *should read* as follows:

Fig. 6. (b) Parallel distorted isotaches with $c^*/b^* = c/b$

The publishers would like to state that the graphs were inaccurately autotraced and redrawn, particularly with regard to Fig. 6(b). The author's attention was not drawn to this.

Sizewell B foundation dewatering—system design, construction and performance monitoring by D. J. Knight, G. L. Smith and J. S. Sutton (1996). *Geotechnique* **46**, No. 3, 473–490

On page 475, Fig. 2, the fill for London Clay, Lower London Tertiaries and Chalk was incorrectly rotated 90°, following approval.